### Source Test Method ST-35

### TOTAL AND HEXAVALENT CHROME

(Adopted January 18, 1989)

#### **REF:** Regulations 11-8-301, 310, 330

#### 1. APPLICABILITY

1.1 This method is used to quantify total and hexavalent chromium emissions. It is applicable to the determination of compliance with Regulation 11-8-301, 310, and 330.

#### 2. PRINCIPLE

2.1 Sample Collection. Chromium emissions are sampled isokinetically from the emission point and collected on Teflon coated disc filters. The materials collected on the filters are then analyzed for total and hexavalent chromium according to Analytical Procedure, Lab-34. If the source is known to emit only hexavalent chromium then only an analysis for total chromium is necessary.

#### 3. RANGE

3.1 Detection Limit. The minimum measurable concentrations of total chromium and hexavalent chromium, by this method, are 8.8 and 7.0 micrograms per cubic meter, respectively.

#### 4. INTERFERENCES

4.1 There are no known interferences for those sources covered by Regulation 11, Rule 8. However, the samples must be extracted, stabilized and analyzed within the time frames specified in Analytical Procedure, Lab-34.

#### 5. APPARATUS

- 5.1 Probe Nozzle. The probe nozzle shall be constructed of borosilicate glass, or quartz with a sharp, tapered leading edge. The angle of the taper shall be 30 degrees and the taper shall be on the outside to preserve a constant internal diameter. The probe nozzle shall be of the button-hook or elbow design. Nozzle diameters shall be sized to allow for isokinetic sampling.
- 5.2 Filter Medium. Use Pallflex Type T60A20 Teflon disc filter or equivalent.
- 5.3 Connections. The connection between the filter and the first impinger must be able to withstand stack temperatures. All connections leading up to the filter should be constructed of Teflon and/or borosilicate glass and/or quartz. Vinyl tubing is acceptable in making all other connections.
- 5.6 Pitot Tube. Use a Stauscheibe (Type-S), or equivalent, with a known coefficient which is constant within  $\pm$  5% over the entire working range. The

pitot tube coefficient is determined by placing both the Type-S and the standard pitot tube in a gas stream and measuring the pressure head with both over the entire velocity range of interest. Calculate the coefficient of the Type-S pitot tube as given by Equation 35-1.

$$C p_{s} = C p_{std} \left[ \frac{\Delta P_{std}}{\Delta P_{s}} \right]^{\frac{1}{2}}$$
 [Equation 35-1]

where:

 $Cp_{S}$  = Type-S pitot tube coefficient, (dimensionless)

 $\Delta P_s$  = Pressure head, Type-S pitot tube, (inches H<sub>2</sub>O)

 $\Delta P_{std}$  = Pressure head, standard pitot tube, (inches H<sub>2</sub>O)

- 5.5 Temperature Measuring Device. Use a Chromel-Alumel thermocouple accurate to  $\pm$  15°F, connected to a temperature compensated null type potentiometer, or equivalent, to measure stack temperatures.
- 5.6 Condensers. Use three Greenberg-Smith impingers. The third impinger shall be modified by removing the impaction plate and attaching a thermometer to the inlet stem.
- 5.7 Cooling System. Use an ice bath to contain the impingers.
- 5.8 Sample Pump. Use a leak-free vacuum pump capable of maintaining a 28.7 lpm (1.0 CFM) flow rate at 380 mm Hg (15 inches of mercury). The pump must have a sample rate control valve and a vacuum gauge attached to the inlet.
- 5.9 Silica Gel Tube. Use approximately 500 cc of silica gel followed by a Drierite indicator, to insure that the gas entering the dry test meter is free of water.
- 5.10 Dry Test Meter. Use a 175 CFH dry test meter accurate within  $\pm$  2% of the true volume and equipped with a thermometer to measure the outlet temperature. The working pressure across the meter shall not exceed one inch of water column.
- 5.11 Rotameter. Use a calibrated rotameter to measure the sampling rate.
- 5.12 Pressure Gauge. Use a Magnehelic differential pressure gauge, or equivalent, in the same range as the velocity and static pressures being measured in the stack.
- 5.13 Analytical Balance. An analytical balance capable of measuring condensate weights to the nearest 0.1 gram is acceptable.
- 5.14 Barometer. Use a barometer that is accurate to within  $\pm$  0.2 inches of mercury.

5.15 Filter Heating System. Use a heating system capable of maintaining a constant temperature around the filter holder, during sampling, of 120  $\pm$  14  $^{\circ}$ C (248  $\pm$  25  $^{\circ}$ F). A temperature gauge accurate to within 3  $^{\circ}$ C (5.4  $^{\circ}$ F) shall be installed such that the temperature around the filter holder can be monitored during sampling.

#### 6. **PRE-TEST PROCEDURES**

- 6.1 Impinger Preparation. Fill the first two Greenberg-Smith impingers with approximately 100 ml of distilled water. Weigh and record the weights on the data sheet as shown in Form 35-1.
- 6.3 Nozzle Size Determination. The nozzle size is determined by the same method described in Section 6.3 of ST-15.
- 6.3 Assembly. Assemble the sampling train as illustrated in Figure 35-1.
- 6.4 Leak Check. The entire sampling train must be leak-checked before each test run. Plug the sampling probe, start the pump, and adjust the pump vacuum to 380 mm Hg (15 inches Hg). A leak rate through the meter which exceeds 0.57 lpm (0.02 CFM) is unacceptable.

#### Figure 35-1



#### **Chromium Sampling Train**

#### 7. SAMPLING

7.1 Test Length. Each test run shall be a minimum of 50 minutes duration when testing emissions from continuous operations. Each test run at batch

process operations shall be for 90% of the batch time or 50 minutes, whichever is less.

- 7.2 Start-up. When inserting the probe into the stack, rotate the nozzle so that it points down stream to avoid particulate collection prior to sampling. Immediately before sampling, rotate the probe so that the nozzle points upstream.
- 7.3 Sample Location. Sample at the traverse points determined in accordance with ST-18.
- 7.4 Data Record. Record the following information at 5 minute intervals or whenever changing sampling locations on a field data sheet as shown in Form 35-2.

Stack Velocity Head Sample time Isokinetic Sample Rate Cumulative Sample Volume Impinger Saturation Temperature Stack Gas Temperature Impinger Vacuum Dry Test Meter Temperature

- 7.6 Saturation Impinger. Add ice as necessary to maintain impinger temperatures at 7°C (45°F) or less.
- 7.7 Shut Down. At the conclusion of each run, stop the pump, remove the probe from the stack and record the final meter reading.
- 7.8 Sample Recovery. Leak-check the sample train as detailed in Section 6.4 of this method. Wash the sample probe, nozzle, filter cap and all tubing leading up to the filter with a maximum of 25 ml of acetone. Save this probe and nozzle wash in chemically inert storage containers for chromium analysis. Remove the filter from the filter holder and place in a clean Petri dish for subsequent chromium analysis.
- 7.9 Repeatability. Three consecutive test runs shall be performed whenever possible. The sample shall be extracted isokinetically ( $\pm$  10%) if the stack gas velocity exceeds 6 ft/sec.

#### 8. POST-TEST PROCEDURES

8.1 Analysis. Analyze the filters and any material in the nozzle for chromium according to Analytical Procedure, Lab 34.

#### 9. AUXILIARY TESTS

9.1 Amp-hour Usage Determinations. If the bath is equipped with a DC ammeter, read and record amperage directly. Otherwise, record power usage into the electroplating rectifier. Record the voltage level supplied to the plating bath. Record the AC to DC efficiency factor through the rectifier.

If no efficiency factor has been determined, then assume a 75% efficiency in power conversion through the rectifier. Calculate the amperage using Equation 35-2.

$$I = \frac{1000 \times e \times P}{E}$$
 [Equation 35-2]

Where:

- e = Power conversion efficiency across the rectifier, (dimensionless)
- E = Voltage to plating bath, (volts)
- I = Amperage through plating bath, (Amps)
- P = Power consumption by rectifier, (Kw)

#### 10. CALCULATIONS

10.1 Standard Dry Sample Volume. Calculate the standard dry sample volume according to Equation 35-3.

$$V_{o} = \frac{530 \times V_{m} \times P_{b}}{29.92 \times T_{m}}$$
 [Equation 35-3]

where:

Pb	=	Barometric Pressure, (inches Hg)
Tm	=	Average Meter Temperature, ( <sup>O</sup> R)
Vm	=	Actual Metered Volume, ft <sup>3</sup>
Vo	=	Standard dry meter volume (dry ft <sup>3</sup> or SDCF)
29.92	=	Standard barometric pressure, (inches Hg)
530	=	Standard temperature, ( <sup>0</sup> R)

10.2 Water Vapor Content. Calculate the water content using Equation 35-4.

$$Wf = \frac{(0.0474 \times W_{c}) + \frac{V_{o} P_{sat}}{(P_{b} - P_{i} - P_{sat})}}{(0.0474 \times W_{c}) + V_{o} + \frac{V_{o} P_{sat}}{(P_{b} - P_{i} - P_{sat})}}$$
[Equation 35-4]

where:

P<sub>b</sub> = Barometric pressure, inches Hg

P<sub>i</sub> = Pump inlet vacuum, inches Hg

- P<sub>sat</sub> = Water saturation pressure in the impingers, inches Hg.
  - Vo = Standard dry sample volume, (ft  $^3$ )
- Wc = Total condensate weight, all impingers, (grams)
- Wf = Water fraction, (dimensionless)

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- 0.0474 = Cubic feet of vapor resulting from 1 cc of liquid water (ft<sup>3</sup>/gram)
- 10.3 Isokinetic Ratio. Isokinetic ratio for sample collection at each traverse point shall be calculated according to Equation 35-5.

$$R_{i} = \frac{(T_{si})(V_{mi})}{60 \times (1 - Wf) \times A_{n} \times V_{si} \times t_{i} \times T_{mi}}$$
 [Equation 35-5]

where:

- R<sub>i</sub> = Isokinetic ratio at traverse point i
- T<sub>si</sub> = Stack temperature at traverse point i, <sup>o</sup>R
- V<sub>mi</sub> = Metered volume at traverse point i, ft<sup>3</sup>
- V<sub>si</sub> = Stack gas velocity at traverse point i, FPS
- t<sub>i</sub> = Time at traverse point i, minutes
- Tmi = Meter temperature at traverse point i, <sup>o</sup>R
- $A_n = Cross-sectional area of nozzle, Ft<sup>2</sup>$
- Wf = Water fraction, (dimensionless)
- 60 = Conversion from seconds to minutes
- 10.4 Hexavalent Chromium concentration. The hexavalent chromium concentration from each test run shall be calculated according to Equation 35-6.

$$C = \frac{35.31 \times W}{1000 \times V_o}$$
 [Equation 35-6]

where:

- C = Hexavalent chromium concentration, (mg/m<sup>3</sup>)
- V<sub>o</sub> = Standard dry sample volume, (SDCF)
- W = Weight of hexavalent chromium per filter plus probe and nozzle wash, (μg)
- $35.31 = \text{Conversion factor, (ft}^3/\text{m}^3)$
- 1000 = Conversion factor, ( $\mu$ g/mg)
- 10.5 Hexavalent Chromium emission rate. The hexavalent chromium emission rate shall be calculated according to Equation 35-7.

$$M = \frac{60 \times (1 \times 10^{-6}) \times W \times Q_{std}}{V_0}$$
 [Equation 35-7]

where:

M = Hexavalent chromium emission rate, (g/hr)

- Q<sub>std</sub> = Standard dry volumetric flow rate exhausting from the stack, (SDCFM)
- V<sub>o</sub> = Standard dry sample volume, (SDCF)
- W = Weight of hexavalent chromium per filter plus probe and nozzle wash, (μg)
- 60 = Conversion factor, (min/hr)
- $1X10^{-6}$  = Conversion factor, (g/µg)
- 10.6 Hexavalent Chromium plating emission factor. Hexavalent chromium emissions per amp-hour shall be calculated according to Equation 35-8.

$$M_{a} = \frac{1000 \times M}{I}$$
 [Equation 35-8]

where:

- M<sub>a</sub> = Hexavalent chromium plating emission factor, (mg/amp-hr)
- I = Amperage determined in section 9.1 of this source test procedure

1000 = Conversion factor, (mg/g)

#### 11. **REPORTING**

11.1 The data and information indicated in Form 35-3 shall be reported.

# Bay Area Air Quality Management District

# Form 35-1

# Source Test Laboratory Data Sheet

## **Impinger Weightings**

Plant Name:	Plant Number:
Source Operation:	Test Date
Source Test #:	Page: 1 of
Impinger Solution:	Initial:

Impinger	( A )	(B)	( C )
I. D. #	Tare Weight (g)	Filled Weight (g)	Final Weight (g)

Impinger	( C-A )	( C-B )	Condensate
I. D. #	Sample Weight (g)	Condensate Wt. (g)	Weight / Run (g)
			Run A
			Run B
			Run C
			Run D

Plant # Bay Area Air Quality Management District							Nozzle I	Diameter							
Source I.D.					939 Ellis Street, San Francisco, CA 94109							Pitot Tube I.D., Cp			
S	ample 7	Гуре					For	m 35-2					Gas Sys	stem	
Pr	ocess C	ycle				Sou	irce Te	st Dat	a Sheet				Pbar, Ba	arometer	
	Duct	Size											 Leak Te	Leak Test Rate	
	Duct Sh	nape			Run #			[	Date:				Time @	Point	
Du	uct Pres	sure		T	Temp Meter #			Box	Box ∆H@			# of Points			
Ass	umed %	6H₂0		M	ag. Gauge #			Met	er (Y)				Time/Ru	ın (Min.)	
Samp	ling Tra	ain: Prob	e #		Filter #		_ Imp. #		Imp	o. #	P	Pump/Box #			
	Init	ial Traverse	e Data						Sam	pling Data					
Trav. Point I.D.	Dist. from Wall	Duct Temp. <sup>°</sup> F	ΔΡ "H <sub>2</sub> 0	Angle of Flow	Traverse Point I.D.	ΔΡ "H <sub>2</sub> 0	Duct Temp. <sup>°</sup> F	Vs FPS	Time (minutes)	Meter Rate CFH	Meter Temp. <sup>0</sup> F	Meter Volume Ft <sup>3</sup>	Train Vacuum "Hg	Sat'd Gas Temp. <sup>0</sup> F	
Post F	Run Imp	inger Cato	:h (ml) =	1		Source	Test Tear	n	Cor	nments:	1	1	1		
-	ľ	Assun	ned $O_2 =$		·	_									
-		Assume	$d CO_2 =$												
Pos	Post Run Calculated %H <sub>2</sub> O =														

Form 35-3								
Distribution:	BAY AREA AIR QUALITY MANAGEMENT DISTRICT				г <sub>т</sub>	Report No.: Test Date:		
Permit Services		939 Ellis Street San Francisco, Californ	a 94109		I	est Times:		
Technical Service	rvices ces	(415) 771-6000 Summary	of			Run A:		
Planning Requester		Summary		40		Run B:		
DAPCO		Source Test	Resur	tS		Run C:		
	Source In	formation		В	AAQME	Representa	tives	
Firm Name and Ad	dress	Firm Representative and Title			e Test Engi	neers		
		Phone No. ( )						
Permit Conditions:		Source:		Permit	t Services D	es Division/Enforcement Division		
		Plant No. Permit Operates	Permit No. Test Requeste		Requested E	əd By:		
Operating Paramet	ters:							
Applicable Reg	ulations:			VN R	ecomme	nded:		
Source Test Re	sults and Comme	nts:						
METHOD TES	Ţ	RUM	IA <u>RI</u>	<u>JN B</u>	<u>RUN C</u>	AVERAGE	<u>LIMIT</u>	
ST-17 Stac	k Volume Flowrate	, SDCFM						
Stac	Stack Gas Temperature, <sup>0</sup> F							
ST-23 Wate	Water Content, Volume %							
ST-35 Tota	Total DC Amps							
Hexa	Hexavalent Chromium, mg/amp-hr							
Hexa	Hexavalent Chromium, g/hr							
Hexa	Hexavalent Chromium, mg/m <sup>3</sup>							
	Isokinetic Ratio, (act/theo)							

Air Quality Engineer II Dat e	Supervising Air Quality Engineer Date	Approved by Air Quality Engineering Manager
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